Rotor5: Rotor design under 5 hours using ultra-fast and high-fidelity CFD simulation and automatic meshing

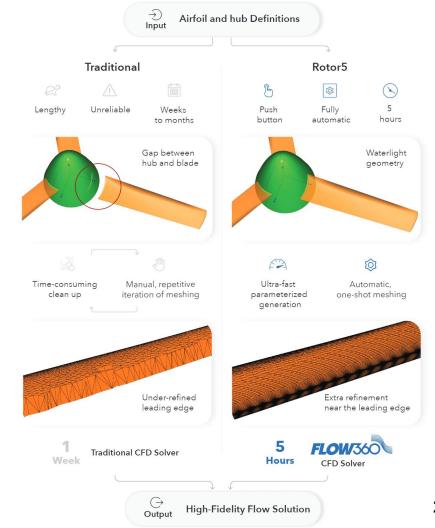


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Introduction

Advantages

- 1. Watertight geometry
- 2. Splitting (but not over-splitting) the patches
- 3. Auto labeling: patches and edges
- Auto meshing (surface and volume)
 Different resolutions for different patches
 Anisotropic layers near given edges





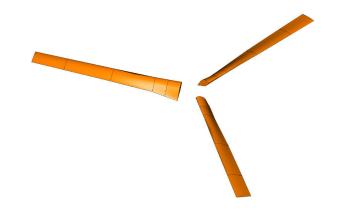


Table 1 Main properties

Parameter	Value
Number of blades, N_b	3
Rotor radius, R	150 inches
Reference blade chord, c_{ref}	14 inches
Aspect ratio, R/c_{ref}	10.71
Rotor solidify, σ	0.089
Linear twist angle, Θ	-40.25°

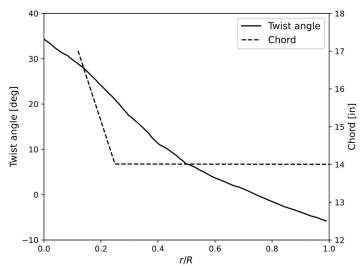


 Table 2
 Airfoil definitions

r/R	Airfoil
0.09	NACA 64-935
0.17	NACA 64-528
0.51	NACA 64-118
0.80	NACA 64-(1.5)12
1.00	NACA 64-208

Freestream Conditions

	Airplane Mode	Hover Mode
Blade-tip Mach number ($M_{\rm tip}$)	0.54	0.69
Reynolds number (Re)	4.50×10^{6}	4.95×10^{6}
Blade pitch angle (θ_{75})	26°,27°,28°,28.8°	0°,3°,5°,10°,13°
Angle of attack (α)	-90°	
Advance ratio	0.337	





Airplane mode

Helicopter mode

Figure of Merit (FoM)

Empty weight

$$W_{\text{empty}} = 4,574 \text{ kg}$$

Maximum gross weight

$$W_{\rm gross} = 6,000 \text{ kg}$$

Take $g = 9.8 \text{ m/s}^2$, thrust from each rotor:

$$T = \frac{1}{2} g W$$

Thrust coefficient

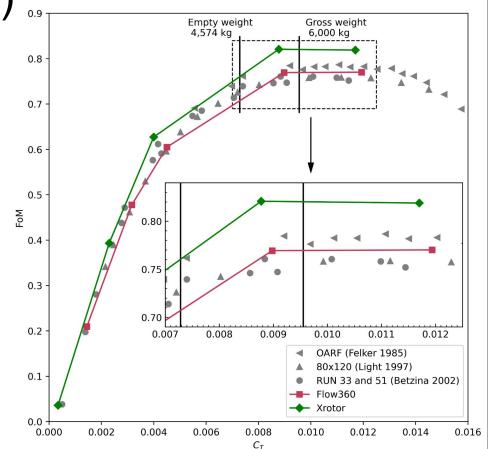
$$C_T = \frac{T}{\rho (\Omega R)^2 A}$$

Torque coefficient

$$C_Q = \frac{Q}{\rho (\Omega R)^2 AR}$$

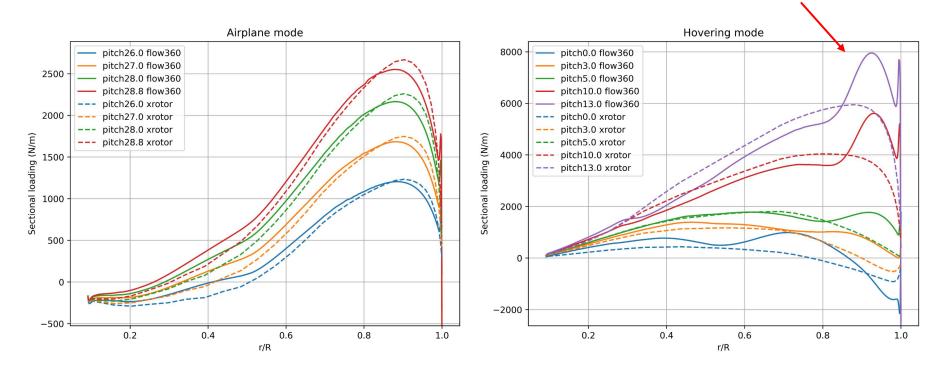
Figure of Merit

$$FoM = \frac{C_T^{3/2}}{\sqrt{2} C_O}$$



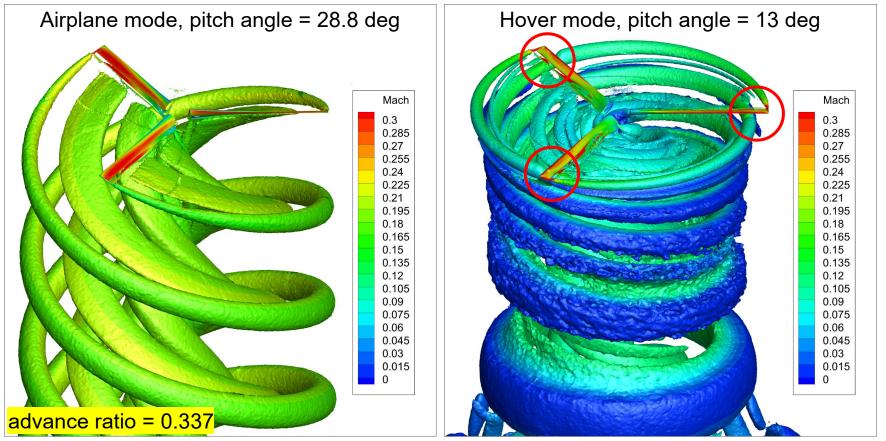
Sectional Loading

Blade-vortex interaction



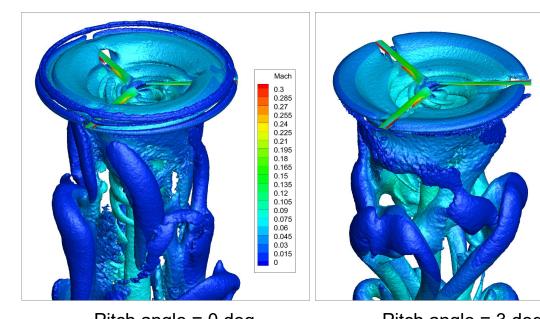
Different colors: different blade pitching angles. Solid and dashed lines: Flow360 and Xrotor results.

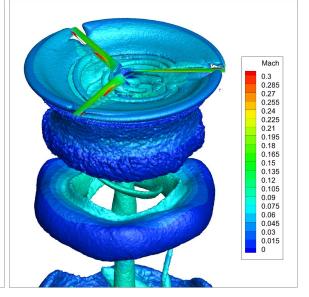
Blade-vortex interaction creates induced drag near the tip and further increases the torque



Isosurface of Q-criterion (Q = 5e-8) colored by Mach number.

Hover Mode, Low Pitch Angles





Pitch angle = 0 deg

Pitch angle = 3 deg

Mach

0.285

0.27

0.255

0.24

0.225

0.21

0.195

0.18

0.165

0.15

0.135

0.12

0.105

0.09

0.075

0.06

0.045

0.03

0.015

0.3

Pitch angle = 5 deg

Downstream Wake

Aixal

Circumferentialy-average axial velocity is given by

$$\overline{v_a}(r) = \frac{1}{2\pi} \int_0^{2\pi} r \, v_a(r,\theta) \, d\theta$$

number of blades

Circumferential

non-dimensional circulation on each blade (denoted as GAM in Xrotor)

Total non-dimensional circulation $|B| \cdot |\Gamma(r)|$ in Xrotor can be written as

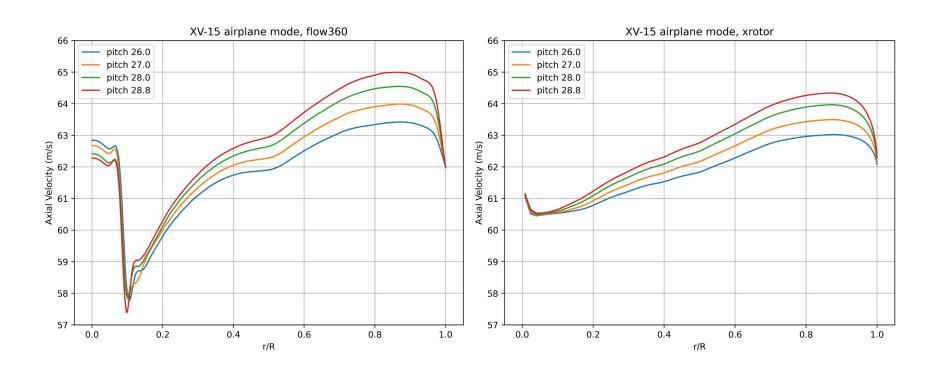
$$B \cdot \Gamma(r) = 2\pi \frac{r}{R} \frac{\overline{v_t(r)}}{V_{\infty}}$$

$$\Rightarrow \overline{v_t(r)} = \frac{B \cdot \Gamma(r)}{2\pi r/R} V_{\infty}$$
circumferentially-averaged tangential velocity

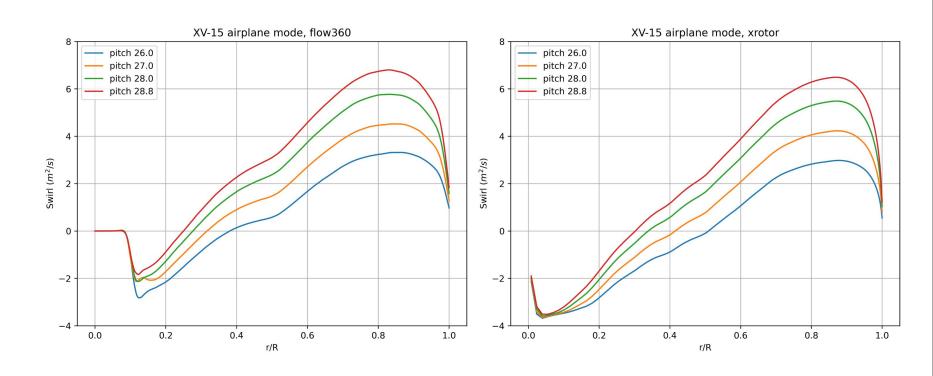
Swirl can be written as

$$S(r) = \frac{1}{2\pi} \int_0^{2\pi} r \, v_t(r,\theta) \, d\theta = r \, \overline{v_t}(r)$$

Airplane Mode, Axial Velocity

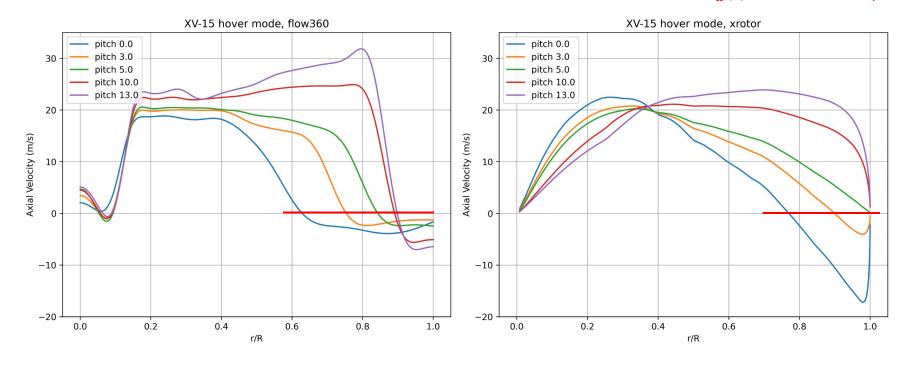


Airplane Mode, Swirl

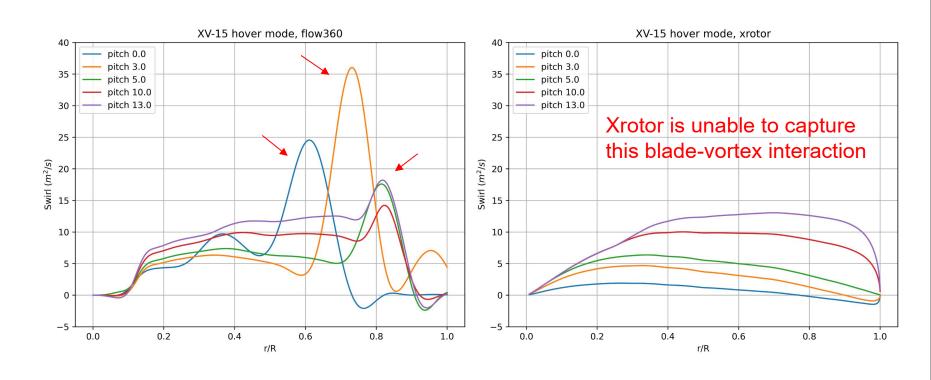


Hover Mode, Axial Velocity

 $\overline{v_a}(r) < 0$ near the tip

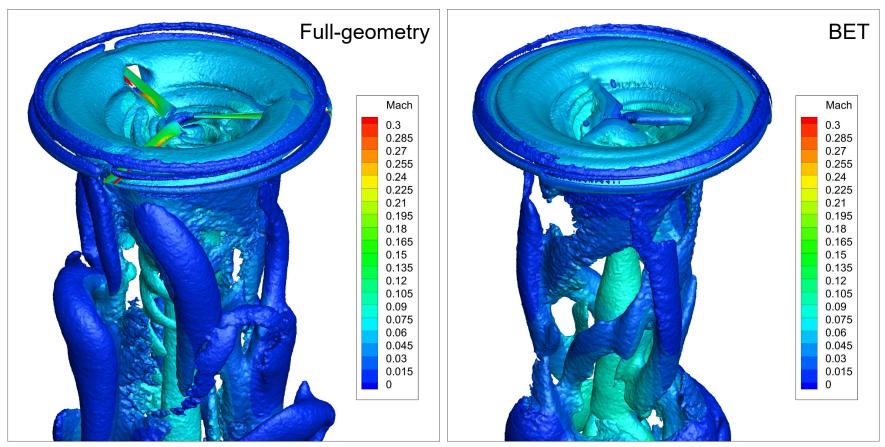


Hover Mode, Swirl

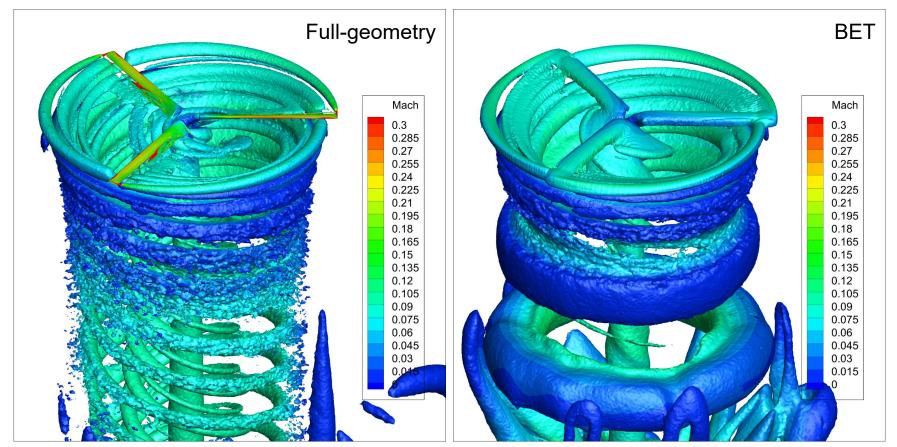




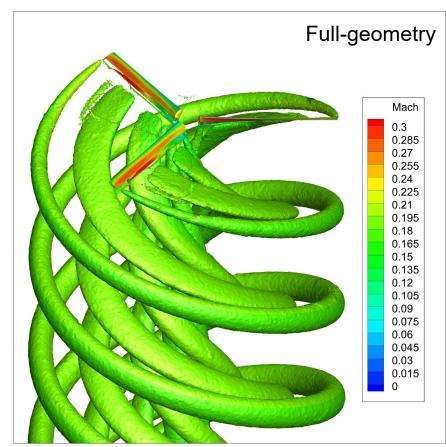
Blade Element Theory

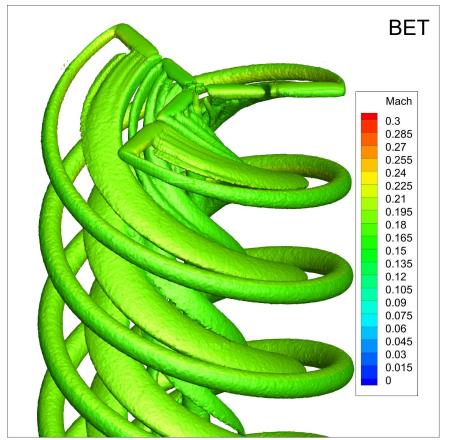


Hover mode, pitch angle = 0 deg (Q = 5e-8)



Hover mode, pitch angle = 10 deg (Q = 5e-8)



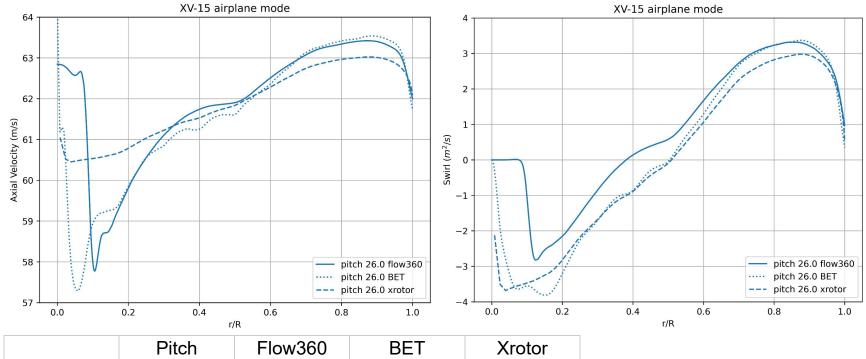


Airplane mode, pitch angle = 26 deg (Q = 5e-8)



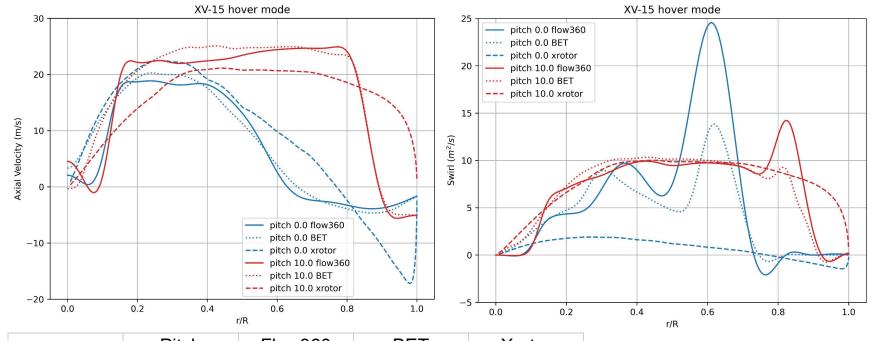
Downstream Wake Comparison Flow360, BET and Xrotor

Airplane Mode



	Pitch	Flow360	BET	Xrotor
Thrust (N)	26.0 deg	3.96E+03	3.19E+03	3.06E+03
Torque (N·m)	26.0 deg	6.43E+03	5.30E+03	4.91E+03

Hover Mode

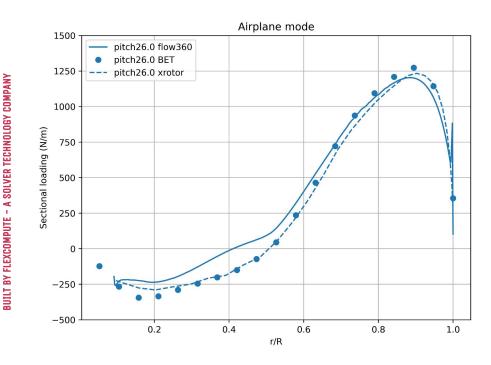


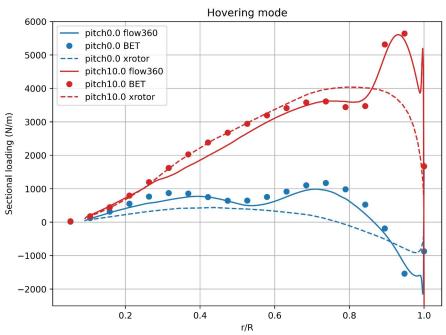
	Pitch	Flow360	BET	Xrotor
Thrust (N)	0.0 deg	4.44E+03	5.06E+03	1.06E+03
Torque (N·m)	0.0 deg	2.17E+03	1.87E+03	1.46E+03
Thrust (N)	10.0 deg	2.76E+04	2.87E+04	2.70E+04
Torque (N·m)	10.0 deg	9.17E+03	8.94E+03	8.29E+03



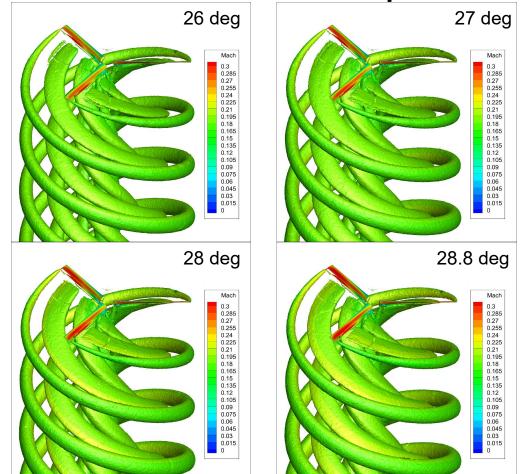


Sectional Loading BET





Q-Criterion Isosurface, Airplane Mode



Q-Criterion Isosurface, Hover Mode

